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54 **Low temperature expandable vermiculite and intumescent sheet material containing same.**

57 A method of decreasing the expansion temperature and improving the expansion characteristics of vermiculite ore comprising subjecting vermiculite ore containing interlamellar cations to a potassium nitrate solution for a time interval sufficient to ion-exchange interlamellar cations within said ore with potassium ions. Subsequent to this ion exchange the low temperature expandable vermiculite may be expanded by heating in an oven, or incorporated in an intumescent material and heat expanded in situ, or expanded by other heating means. An intumescent sheet is provided which may be used for mounting automotive catalytic converter monoliths comprising an unexpanded vermiculite produced by the method of the invention; an inorganic fibrous material; and a binder.

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LOW TEMPERATURE EXPANDABLE VERMICULITE AND INTUMESCENT SHEET MATERIAL CONTAINING SAME

The present invention relates to a method of treating vermiculite ore to lower the expansion temperature of the ore and improve the characteristics of the expanded vermiculite. The invention is further directed to intumescent sheet and other intumescent materials containing low temperature expandable vermiculite prepared according to the invention.

5 Vermiculite is a micaceous mineral, chemically identified as a hydrated magnesium-aluminum-iron silicate and characterised by a layered structure which exfoliates or expands in one dimension when heated at high temperatures or subjected to various chemical treatments, so as to be increased to many times its original size. The mineral ore occurs naturally in an unexpanded state, and is mined in conventional manner.

10 Since vermiculite as it is mined in the form of vermiculite ore is associated with other minerals as impurities, the crude vermiculite ore, after being reduced to particle size, generally in the form of flakes, has generally been beneficiated by various concentrating methods well known in the art wherein the gangue material is separated from the vermiculite particles as much as possible, the vermiculite screened into a number of component sizes and the vermiculite heated at elevated temperatures, typically approximately 15 982° C (1800° F), until expansion occurs.

It has been an important goal to find a means and method of lowering the expansion temperatures of vermiculite ore, both for economic reasons, and so that the vermiculite may be used in applications where a material is required which may be expanded in situ at relatively low temperatures. However, at lower expansion temperatures untreated vermiculite either will not expand at all, or will not yield an acceptable 20 volume of expanded product.

It is known to increase the volume yield of vermiculite, and slightly decrease the expansion temperature, by osmotically swelling the vermiculite ore prior to expansion by treating the ore with various solutions containing alkali or alkaline earth salts. Such a method is described in U.S. Pat. No. 3,062,753. This method succeeds in increasing the yield of the ore, but the expansion temperature is still uneconomical and too 25 high for the vermiculite to be used in many applications.

This method, and other previously known methods of treating vermiculite with salt solutions, also have several accompanying disadvantages. First, intumescent materials containing the expandable vermiculite thus produced tend to shrink upon initial heating, especially when the vermiculite is incorporated in intumescent gasket materials and expanded in situ under load, (this shrinkage is generally referred to in the 30 art, and will be referred to herein, as "negative expansion"). This negative expansion may be deleterious in some applications, e.g. intumescent gasketing applications where it may interfere with the formation of a tight seal. Secondly, the disposal of the solutions used must be carefully monitored, especially when the salt used is an alkali or alkaline earth chloride, as these solutions are considered potentially hazardous to the environment. Furthermore, the residual chloride ions contained in the expanded vermiculite may be 35 corrosive in certain applications and are undesirable in agricultural and horticultural applications.

The expansion temperature of vermiculite ore may be lowered, and the tendency of the sheet containing the vermiculite to undergo negative expansion reduced, by treating the vermiculite ore with ammonium cations, as disclosed in U.S. Patent No. 4,305,992, the disclosure of which is incorporated herein by reference. However, the ammonium solutions used in this process tend to be relatively costly, 40 and the disposal of the resulting waste stream also must be closely monitored as the waste is potentially hazardous. Also, the expansion temperatures thus obtained are still too high for many applications in which it would be desirable to use vermiculite.

It has been desired to use vermiculite in materials which are designed to expand when exposed to heat, i.e. intumescent materials. These intumescent materials are used in many applications including fireproofing 45 insulation and gasketing. Vermiculite is also useful in fireproofing materials referred to as endothermic materials, which block heat penetration by absorbing energy chemically. Intumescent sheet materials containing vermiculite generally comprise vermiculite, inorganic and organic fibers, low density fillers, e.g. hollow glass microspheres, and organic binders. Vermiculite is useful in these applications both because it expands when exposed to heat, typically from 8 to 20 times, and thus can seal flames and heat out of 50 openings, ducts, and other areas, and because of its ability to block heat penetration by absorbing energy via chemically bound interlayer water and other volatile.

An intumescent sheet comprising unexpanded ammonium, ion exchanged vermiculite, inorganic fibrous materials and binders is disclosed in the aforementioned U.S. Patent No. 4,305,992. This flexible intumescent sheet material is utilised in automobile exhaust catalytic converters as a mounting material by

expansion in situ. The expanded sheet then holds the ceramic core or catalyst support in place in the container or canister. The thermal stability and resilience of the sheet after exfoliation compensate for the difference in thermal expansion of the metal canister and the ceramic substrate, for vibration transmitted to the fragile device and for irregularities in the metallic or ceramic surfaces. Generally, in this application
 5 intumescent sheets are expanded in situ by the catalytic converter manufacturer by connecting the converter to an automobile exhaust system and running the automobile until the intumescent sheet expands fully.

One disadvantage of conventional intumescent materials is that they generally undergo negative expansion when exposed to temperatures of from 110 to 399°C (230°F to 750°F). In gasket applications,
 10 such as the packing and mounting of automobile catalytic converters, this negative expansion may cause the mounted catalyst support to become undesirably loose when these temperatures are encountered and remain loose until such time as the intumescent sheet material has passed through the negative expansion region and expanded sufficiently to recover its original thickness.

The present invention relates to a method of creating vermiculite ore to lower the expansion temperature of the ore and provide improved properties to the vermiculite. The invention is further directed to
 15 intumescent materials, and particularly intumescent sheet materials, containing low temperature expandable vermiculite prepared according to the invention, which vermiculite expands within the intumescent material at advantageously low temperatures and exhibits minimal negative expansion.

More particularly, the present invention provides a method of treating vermiculite ore containing
 20 interlamellar cations comprising contacting vermiculite ore containing interlamellar cations with a potassium nitrate solution for a time interval sufficient to ion-exchange interlamellar cations within said ore with potassium ions.

The low temperature expandable vermiculite thus produced may be thermally expanded using conventional apparatus such as expansion ovens well known in the art. Alternatively, the vermiculite may be
 25 incorporated in an intumescent material, such that the vermiculite will expand in situ when the intumescent material is exposed to sufficient heat.

The present invention further relates to an intumescent sheet containing the low temperature expandable vermiculite of the invention. More particularly, the present invention relates to a flexible intumescent sheet which may be used for mounting automotive catalytic converter monoliths comprising an unexpanded
 30 vermiculite produced by subjected vermiculite ore containing interlamellar cations to a potassium nitrate solution for a time interval sufficient to ion-exchange interlamellar cations within said ore with potassium ions; an inorganic fibrous material; and a binder. This sheet will expand quickly at a relatively low temperature, saving production time and gasoline for the manufacturer and reducing the exhaust produced in the factory per converter. In a preferred embodiment, the flexible intumescent sheet comprises from 20%
 35 to 80%, and preferably from 40% to 65% by weight of the ion exchanged vermiculite, from 25% to 50% by weight of the fibrous material, and from 5% to 15% by weight of the binder.

The intumescent materials of this invention may also advantageously be used in fireproofing and heatproofing applications due to the high level of bound volatiles in the vermiculite, and thus the endothermic nature of the treated vermiculite contained in the sheet.

The term vermiculite, as it is used herein, refers to the group of rock forming mineral species characterised by a layer latticed structure in which the silicate layer units have a thickness of approximately 10 angstroms. The main elements present in the layer are magnesium, aluminum, silica, iron and oxygen with the layers being separated by one or two sheets of water molecules associated with cations such as
 40 magnesium, calcium, sodium and hydrogen. The layers have considerable lateral extent relative to the thickness of the basic 10 angstrom unit layer. The term vermiculite as used herein therefore includes minerals consisting wholly or largely of vermiculite, or minerals of a mixed-layer type containing vermiculite layers as an important constituent, such as hydrobiotites, and chlorite-vermiculite, but does not include minerals of the montmorillonite group.

Heretofore, the degree to which the expansion temperature is lowered by ion exchanging the vermiculite with a given salt solution has been attributed primarily to the type of cation present in the solution. The anion component of the salt has been given less consideration, and has conventionally been chloride. Unexpectedly, it has been found by the inventors that the expansion temperature and characteristics of the cation exchanged vermiculite can be determined by the combination of cation and anion used. In particular,
 45 it has been found that the use of the nitrate salt of potassium provides substantial improvements in both the yield of expanded vermiculite and the expansion characteristics, as opposed to that obtained with other potassium salts and other anionic components. Thus, as shown in Example 1, potassium nitrate exchanged vermiculite has, after expansion at a given temperature, a significantly lower bulk density, and thus higher yield, than ammonium nitrate or potassium chloride exchanged vermiculite. Example 1 also shows that
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superior yields can be obtained when potassium nitrate exchanged vermiculite is expanded at temperatures as low as 246° C (475° F), whereas higher temperatures are required to obtain equivalent yields with ammonium nitrate or potassium nitrate exchanged vermiculite. Generally, when potassium nitrate exchanged vermiculite is expanded at 246° C (475° F) or above the resulting bulk density is less than 481 kg/m³ (30 lbs/ft³). The use of a potassium nitrate solution is also desirable from the standpoint of disposal, as this solution can be recycled as a fertiliser without risk to the environment.

The potassium ion exchange generally takes place by subjecting the vermiculite ore to an aqueous solution of potassium nitrate. The concentration of the potassium nitrate solution is preferably from 0.1 to 5 molar, and most preferably from 0.5 to 2.5 molar. When ammonium ion exchange is performed, the optimal concentration is generally 5 molar, making potassium nitrate significantly more cost effective.

The optimum duration of ion exchange is directly dependent on the concentration and temperature of the potassium nitrate solution. Generally, the duration of the ion exchange is from 0.5 to 72 hours, and preferably from 10 to 36 hours. The preferred exchange conditions for a 1 molar solution are 24 hours at room temperature. However, shorter exchange times at higher temperatures may be used, e.g. 4 hours at 93° C (200° F). When weaker solutions are used longer exchange times may be necessary to achieve the same yield.

The weight ratio of vermiculite to salt solution also influences the expansion characteristics of the ion exchanged vermiculite. Preferred ratios are from about 0.5:1.5 to about 1.5:0.5, with the most preferred ratio generally being about 1:1.

It is generally preferred that the excess solution be decanted and the vermiculite be rinsed subsequent to ion exchange in order to remove any excess salt. The vermiculite may be rinsed with distilled water, and it is preferred that the vermiculite be rinsed several times. It is also preferred that the vermiculite be dried prior to expansion. Generally the vermiculite is allowed to air dry at room temperature. The cation exchanged vermiculite of the invention may then be expanded using conventional techniques and equipment.

Generally, the expansion temperature of vermiculite which has been cation exchanged with potassium nitrate is lower than the expansion temperatures of similar vermiculite ore which has been treated under similar conditions with other salt solutions. For example, initial expansion temperatures of intumescent sheets containing vermiculite which had been cation-exchanged under similar conditions with potassium nitrate, ammonium nitrate, potassium chloride, and ammonium chloride, as measured using Thermal Mechanical Analysis, were approximately 246° C, 254° C, 271° C and 271° C (465° F, 490° F, 520° F and 520° F), respectively.

For advantageous yields it is preferred to expand the vermiculite of the invention at a temperature of at least 246° C (475° F), and most preferably in the range of from 246 to 316° C (475° F to 600° F). The minimum expansion temperature of the cation exchanged vermiculite, and the preferred temperature for full expansion, will depend on the type and grade of vermiculite used, due to differences in the mineral and moisture contents of the ores. The expansion process proceeds very quickly; for example within 10 minutes full expansion is generally obtained.

The flexible intumescent sheet material according to the invention comprises unexpanded vermiculite prepared according to the invention, one or more inorganic fibrous materials, and one or more binders. Preferably, the intumescent sheet of the invention comprises from about 40% to 65% potassium nitrate exchanged vermiculite, from about 25% to 50% of the fibrous material, and from about 5% to 15% of the binder.

Inorganic fibrous materials which may be used include glass fibers, slag, rock and ceramic fibers. A preferred fibrous material is ceramic fibers.

Suitable binders can include various polymers and organic elastomers in latex form, as for example, natural rubber latexes, styrene-butadiene latexes, butadiene-acrylonitrile latexes, latexes of acrylate and methacrylate polymers and copolymers and the like.

The sheet material may be formed by standard papermaking techniques, either hand laid or machine laid, taking suitable precautions to attain substantially uniform distribution of particles throughout the web. The sheet material may be provided with or temporarily laminated to a backing sheet of kraft paper, plastic film, non-woven synthetic fiber web or the like as desired. Generally, the potassium nitrate treated vermiculite is combined in a large volume of water with the fibrous material and binder. Small amounts of surfactants, foaming agents and flocculating agents may also be added before forming the sheet. The sheet is then formed by standard papermaking techniques either in a hand-sheet former or Fourdrinier screen. The resulting green sheet is compressed to give a dry weight density of generally at least 0.35 g/ml, and dried at relatively low temperature, generally less than about 90° C, to form a handleable, flexible sheet material.

After drying, the intumescent sheet may be employed in any application where it is desired to employ a

heat expandable, heat resistant sealing or filling material. A preferred use for the intumescent sheets of the invention is as a packing for mounting and positioning automotive catalytic converter monoliths. The intumescent sheet, when used in this application, is wrapped around a catalytic converter core, and the core and sheet are placed inside an outer metal canister. The resulting assembly is then usually mounted in an automobile in standard fashion and heated, generally by the engine exhaust gases, to expand the intumescent sheet. Using the intumescent sheet of the invention, the sheet will generally expand upon reaching a temperature of approximately 246 °C (475 °F).

Intumescent sheets produced according to the invention generally have initial expansion temperatures in the range of from 204 to 316 °C (400 °F to 600 °F), have a maximum negative expansion of about 5% at about 246 °C (475 °F), and return to at least original thickness at about 249 °C (480 °F). These properties are better than those obtained with intumescent sheets produced with vermiculite which has been treated with other salt solutions, as measured by Thermal Mechanical Analysis.

The following examples are intended to be illustrative only and not of limiting effect.

Example 1

Four samples of a vermiculite ore were cation exchanged for 24 hours at room temperature with 1 molar solutions of potassium nitrate, ammonium nitrate, potassium chloride and ammonium chloride, respectively. The cation exchanged vermiculites were then each rinsed five times with distilled water after the excess salt solution was decanted, and then allowed to air dry at room temperature until substantially dry.

Each vermiculite sample was then separated into three batches, one of which was expanded at 246 °C (475 °F), one at 277 °C (530 °F), and one at 316 °C (600 °F). All samples were expanded in a conventional expansion oven. After expansion, the samples were tested for bulk density, with results as shown in Table 1.

The data of Table 1 show that the expanded vermiculite which had been cation exchanged with potassium nitrate had significantly lower bulk density, and thus was more fully expanded, after expansion at a given temperature than the vermiculite which had been cation exchanged with other salts. Further, the bulk density obtained for the potassium nitrate treated vermiculite which was expanded at 246 °C (475 °F) was much lower than that of the other samples which were expanded at the same temperature, and equivalent to the bulk density obtained for the other samples which were expanded at 277 °C (530 °F), indicating a lower initial expansion temperature and more complete expansion at the low expansion temperature.

TABLE 1

Sample	Treated With	Bulk Density (kg/m ³) (lb/ft ³) When Expanded at		
		246 °C (475 °F)	277 °C (530 °F)	316 (600 °F)
1	KNO ₃	389 (24.3)	237 (14.8)	176 (11.0)
2	NH ₄ NO ₃	719 (44.9)	389 (24.3)	274 (17.1)
3	KCl	998 (62.3)	384 (24.0)	272 (17.0)
4	NH ₄ Cl	990 (61.8)	722 (45.1)	365 (22.8)

Example 2

A 2 kilogram batch of vermiculite ore was separated into two 1 kilogram samples, which were exchanged for 24 hours at room temperature with 1 molar solutions of potassium nitrate and ammonium chloride, respectively. The solutions were then decanted from the samples and each sample was dried overnight at 60 °C (140 °F).

Next, two intumescent sheets were identically prepared using the procedure described below, one using the potassium nitrate exchanged vermiculite, and the other using the ammonium chloride exchanged vermiculite.

In a blender, 15.4 grams of alumina-silica ceramic fibers (washed Fiberfrax available from the

Carborundum Co.) were added to 1000 ml of water and agitated. The mixture was then transferred to a beaker and 10 ml of a 0.1% solution of sodium acrylate/acrylamide copolymer surfactant (commercially available from Allied Colloids under the tradename Percol 166) and 10 ml of a 0.1% solution of a quaternary acrylate salt/acrylamide copolymer surfactant (Percol 292) were added. The mixture was then stirred with a mechanical stirrer at a low speed. To this mixture, 28 grams of vermiculite (see above), and 8 grams Hycar 1562X103 (a 40% solution of butadiene-acrylonitrile latex, commercially available from B.F. Goodrich Chemical Co.) were added, and the mixture was again mixed at a low speed. The mixture was then returned to the blender and flocculated with a 10% aluminum sulfate solution (sufficient to reduce the pH to a range of 4.5-5).

The resulting slurry was poured into approximately 1.3cm (0.5 inch) of water in an 19.2cm (8 inch) diameter hand sheet former available from Valley Iron Works, Appleton, WI) and the water drawn off. The wet intumescent paper thus produced was then dried on a steam table.

The relative expansion of the two papers was tested as follows. The initial thickness of the intumescent paper (T_0) was measured using an Ames AD1-71 thickness gauge with the spring removed and an external 28 gram weight added. The paper was then expanded at a given temperature (see Table 2) in a conventional forced air oven for 60 minutes. The expanded thickness (T_E) was then measured using the procedure described above. The relative expansion (T_E/T_0) was then calculated for each sample, with results as shown in Table 2. The data of Table 2 indicates that while the relative expansions of the two papers are similar when expanded at 177° C (350° F), the papers containing the potassium nitrate expanded vermiculite expanded significantly more than those containing ammonium chloride exchanged vermiculite at both 204° C (400° F) and 232° C (450° F).

Table 2

Intumescent Sheet Containing	T_E/T_0		
	177° C	204° C	232° C
KNO ₃ Exchanged Vermiculite	1.14	1.94	2.71
NH ₄ Cl Exchanged Vermiculite	1.18	1.25	1.57

Example 3

Four different batches of vermiculite ore were provided. Each vermiculite batch was separated into two samples (samples 1-8 in Table 3). Samples 1, 3, and 5 were cation exchanged for 24 hours at room temperature with a 1 molar solution of potassium nitrate, samples 2, 4, and 6 were cation exchanged for 24 hours at room temperature with a 1 molar solution of ammonium chloride, and samples 7 and 8 were cation exchanged for 24 hours with 0.5 molar solutions of potassium nitrate and ammonium chloride, respectively. The cation exchanged vermiculites were rinsed and then partially dried.

Each vermiculite sample was then separated into two portions, one of which was dried at 60° C (140° F) for 20 hours (D_{LT}), and the other of which was dried at 885° C (1625° F) for 2 minutes (D_{HT}). The low temperature drying volatilised the loosely bound or adsorbed volatiles in the vermiculite, while the high temperature drying volatilised both loosely bound/adsorbed and tightly bound volatiles. The difference in weight loss obtained using the two drying processes ($D_{HT} - D_{LT}$), indicates the amount of tightly bound interlayer volatile contained in the vermiculite.

The data of Table 3 shows that for a given batch of ore, the tightly bound interlayer volatile level (percent interlayer volatile, $(D_{HT} - D_{LT})$) is greater for potassium nitrate exchanged vermiculite than for ammonium chloride exchanged vermiculite. The percent interlayer volatile of vermiculite which has been cation exchanged in a given solution can vary from one batch of vermiculite ore to another, as seen in Table 3, due to mineralogical, morphological, compositional and other differences between ores.

Table 3

Sample	Exchange Solution	Batch	D _{HT} %	D _{LT} %	D _{HT} -D _{LT} %
1	KNO ₃	1	17.2	3.2	14.0
2	NH ₄ Cl	1	16.9	7.9	9.0
3	KNO ₃	2	10.8	0.4	10.4
4	NH ₄ Cl	2	7.7	0.4	7.3
5	KNO ₃	3	15.8	7.4	8.4
6	NH ₄ Cl	3	6.0	0.4	5.6
7	KNO ₃	4	16.0	1.3	14.7
8	NH ₄ Cl	4	7.8	1.1	6.7

Claims

1. A method of treating vermiculite ore comprising contacting vermiculite ore containing interlamellar ions with a potassium nitrate solution for a time interval sufficient to ion-exchange interlamellar cations within the vermiculite ore with potassium ions.
2. A method according to claim 1 further comprising subsequently decanting the excess solution and rinsing to remove excess potassium nitrate.
3. A method according to claim 2 further comprising subsequently drying the ion exchanged vermiculite ore until substantially dry.
4. A method according to any preceding claim wherein the concentration of the potassium nitrate solution is from 0.1 to 5 molar.
5. A method according to any preceding claim wherein the vermiculite is subjected to the potassium nitrate solution for a period of from 0.5 to 72 hours preferably for a period of from 10 to 36 hours.
6. A method of expanding vermiculite ore comprising the sequential steps of:
 - a) treating the vermiculite ore according to any of claims 1 to 5; and
 - b) heating the ion exchanged vermiculite such that the vermiculite expands.
7. A method of claim 6 wherein the ion exchanged vermiculite is heated in an oven.
8. A method according to claim 6 or claim 7 further comprising incorporating the ion exchanged vermiculite into an intumescent sheet prior to step b).
9. A method according to any of claims 6 to 8 wherein the vermiculite is heated at a temperature of from 246 to 316 °C (475 °F to 600 °F).
10. A method according to any of claims 6 to 9 further comprising decanting the excess potassium nitrate solution and rinsing the ion exchanged vermiculite prior to step b).
11. A method according to any of claims 6 to 10 further comprising drying the vermiculite until substantially dry prior to heating the vermiculite.
12. A method according to any of claims 6 to 11 wherein the expanded vermiculite produced by said method has a bulk density of less than 481 kg/m³ (30 lbs/ft³).
13. A flexible intumescent sheet comprising:
 - a) an unexpanded vermiculite produced according to any of claims 1 to 5
 - b) an inorganic fibrous material; and
 - c) a binder.
14. An intumescent sheet according to claim 13 comprising from 40% to 65% by weight of the unexpanded vermiculite and/or from 25% to 50% by weight of the inorganic fibrous material and/or from 5% to 15% by weight of the binder.
15. An intumescent sheet according to claim 13 or claim 14 wherein the inorganic fibrous material is ceramic fibres.
16. An intumescent sheet according to any of claims 13 to wherein the binder is an organic elastomer.
17. Use of a sheet according to any of claims 13 to 16 or any of claims 9 to 12 when dependant upon claim 8 as a heat expandable, heat resistant sealing or filling material, preferably as a packing for mounting and positioning catalytic converter monoliths.



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EUROPEAN SEARCH REPORT

Application Number

EP 90 31 2440

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)
A	EP-A-0 245 929 (CORNING GLASS WORKS) * page 3, line 36 - page 4, line 28; claims 1-3, 9, 10 * - - -	1-3,6,9	C 04 B 14/20 C 01 B 33/34 F 01 N 3/28
D,A	EP-A-0 030 123 (MINNESOTA MINING AND MANUFACTURING CO) * claims 1-7 * - - -	1,6,13-17	
A	CHEMICAL ABSTRACTS, vol. 81, 1974 Columbus, Ohio, & JP-A-7434915 (TAKEDA CHEMICAL INDUSTRIES LTD) 30-03-1974 page 276; ref. no. 53771F * abstract * - - -	1,6,7	
A	EP-A-0 115 397 (CORNING GLASS WORKS) * page 7, lines 17 - 28; claims 1, 3 * - - -	1-3,6	
A	CHEMICAL ABSTRACTS, vol. 106, no. 24, June 1987 Co- lumbus, Ohio, USA & JP-A-6246978 (NIPPON REINS CO.) 28-02-1987 page 279; ref. no. 200683U * abstract * - - -	13-17	
A	US-A-4 786 620 (H.RITTLER) * claims * - - -	1	TECHNICAL FIELDS SEARCHED (Int. Cl.5)
D,A	US-A-3 062 753 (J.C.HAYES) * column 3, line 7 - column 4, line 32 * - - -	1-3,6	C 04 B F 01 N D 21 H C 01 B
A	PATENT OFFICE OF JAPAN FILE SUPPLIER JAPS & JP-A-59230737 (IBIDEN KK) 25-12-84 - - - - -		
The present search report has been drawn up for all claims			
Place of search The Hague		Date of completion of search 13 February 91	Examiner THEODORIDOU E.
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons ----- & : member of the same patent family, corresponding document			